

■ Air leak test equivalent to IPX7 and IPX8

● In order to perform quantitative tests

Fig. 1 shows the relationship between air leak amount and water leak amount.

Water leak amount can be converted into air leak amount. By performing an air leak test accommodating a water leak allowance equivalent to IPX7 and IPX8, quality control using air leak amount (numerical) is possible, and there is a better chance of preventing waterproof defective products from leaking out to customers.

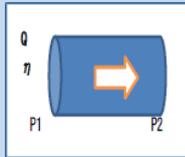
● A water leak amount with “no harmful effect”

IPX7 and IPX8 are designated as “Ingress of water in quantities causing harmful effects shall not be possible.” There is a need to determine the water leak amount (permissible amount which has no harmful effect. If this value is stipulated, waterproof tests within air leak tests will be possible.

Below is an introduction on how air converted amount is found presuming two types of leak hole models (orifice and straight pipe) and assuming a water leak permissible amount of 0.09 mL/30 minutes.

【Straight pipe model】

According to the Hagen–Poiseuille law,
 $Q_a/Q_w = (\eta_w/\eta_a) \times (P_1 + P_2) / (2 \times P_2)$



Viscosity coefficient $\eta_w = 1.00 \times 10^{-3} \text{ Pa sec } 20^\circ\text{C}$
 $\eta_a = 1.81 \times 10^{-5} \text{ Pa sec } 20^\circ\text{C}$

Upward pressure P1 $1.11 \times 10^5 \text{ Pa abs}$
 (absolute pressure reference)

Downward pressure P2 $1.01 \times 10^5 \text{ Pa abs}$

Average pressure $1.06 \times 10^5 \text{ Pa abs}$

$Q_a/Q_w = 58.0$

If the permissible limit of water leak amount (Q_w) was assumed to be 0.09 mL/30 minutes ($Q_w = 5 \times 10^{-11} \text{ m}^3/\text{s}$), the air volume flow rate would be $Q_a = 2.9 \times 10^{-9} \text{ m}^3/\text{s}$.

The air leak amount would then be found by multiplying the average pressure, therefore $3.1 \times 10^{-4} \text{ Pa} \cdot \text{m}^3/\text{s}$ ($\Delta P = 9.8 \text{ kPa}$).

【Orifice model】

According to the orifice flow formula (JIS8762-2)

$$Q_a/Q_w = \varepsilon \times \sqrt{\rho_w / \rho_a}$$

(ε : expansion compensation coefficient)

If the below is the case;

P1 upward pressure $1.11 \times 10^5 \text{ Pa abs}$

P2 downward pressure $1.01 \times 10^5 \text{ Pa abs}$

Water density $\rho_w = 997 \text{ kg/m}^3$ at 25°C

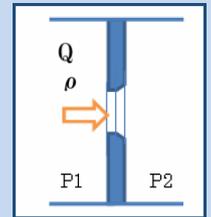
Air density $\rho_a = 1.25 \text{ kg/m}^3$ at 25°C

then $Q_a/Q_w = \varepsilon \times 28.3 = 28.3$

(Assuming that P1 and P2 are close then $\varepsilon = 1 \dots$ JISZ8762-2)

If the permissible limit of water leak amount (Q_w) was assumed to be 0.09 mL/30 minutes, from $Q_w = 5 \times 10^{-11} \text{ m}^3/\text{s}$, the air volume flow rate would be $Q_a = 1.4 \times 10^{-9} \text{ m}^3/\text{s}$.

The air leak amount would then be found by multiplying the average pressure, therefore $1.5 \times 10^{-4} \text{ Pa} \cdot \text{m}^3/\text{s}$ ($\Delta P = 9.8 \text{ kPa}$)



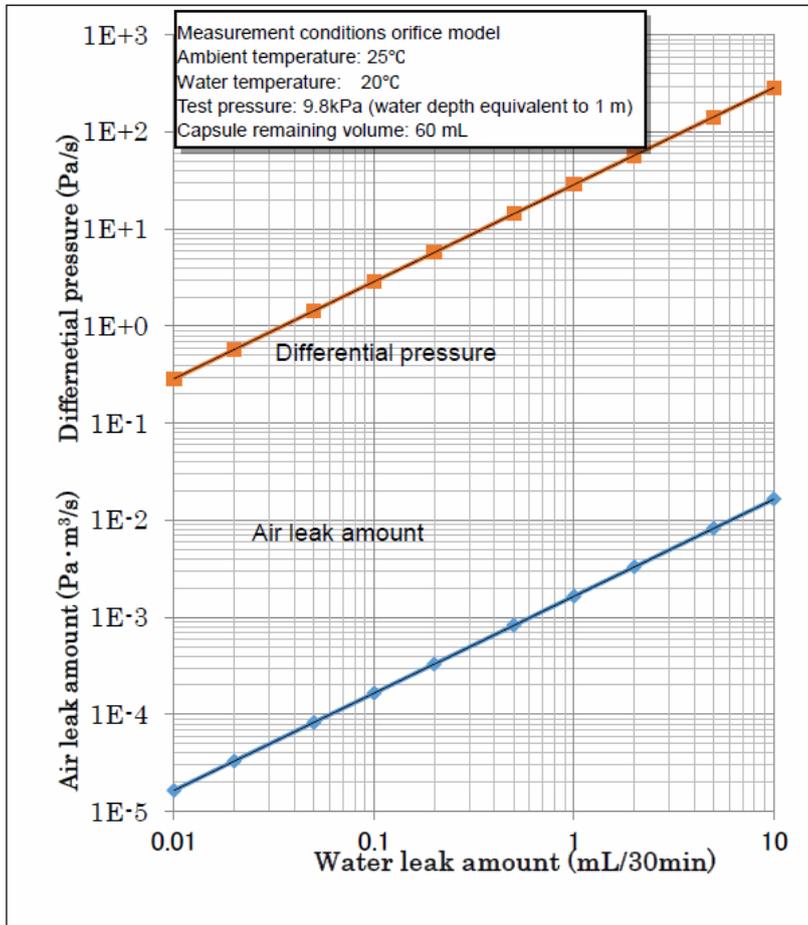
Average pressure
 $1.06 \times 10^5 \text{ Pa abs}$

* Please refer to Page 3~7 “Reference Material” for the theoretical formulas used here.

• Measurement value with an air leak tester presuming an IPX7-equivalent test is performed.

Compared with the straight pipe model, the orifice model uses conditions whereby air leaks and water leaks could easily occur, therefore the orifice model air leak amount and water leak amount ratio of $Q_a/Q_w = 28$ is applied and the relationship between air/water leak amounts is shown in the below figure.

Fig. 1 Relationship between air leak amount and water leak amount



Reference Material

Refer to FUKUDA Technical Manual P.6~9

Leakage of Gas or Fluid (Viscous Flow)

Leakage is a phenomenon which occurs when a fluid such as air, water, or oil passes through an unintended opening such as a small hole. A resultant leak volume differs according to the difference of pressure across the opening; and relates with the ease of fluid flow through the opening; conductance.

This can be expressed by the following equation.

$$Q = C (P_1 - P_2) \text{-----(1.1)}$$

Where Q is leak volume, $P_1 - P_2$ represents the difference between two pressures, and C is conductance. When leakage is the subjective problem, the ease of fluid flow (C) depends on a variety of factors, including the configuration of the opening, length, etc. It is therefore difficult to apply one type of equation to all cases. In this section, an explanation is given using general application equations.

Theoretical Equation of Leak Volume

As a representative theoretical equation to explain the behavior of fluids passing through a very narrow opening, the Hagan-Poiseuille Law is often used. According to this law if the opening is so small that the flow of fluid is within a range of viscous flow (laminar flow), and the ratio of the hole length vs. the hole diameter is large enough, the following equation can be applied;

$$Q_a = \frac{\pi R^4 (P_1^2 - P_2^2)}{16\eta_a \ell P_2} \text{-----(1.2)}$$

Where Q_a is the volumetric flow of outlet side pressure (atmospheric pressure) converted from compressible fluid such as air.

However, if P_1 is negative, the leak volume is expressed in terms of the state of atmospheric pressure. The P_2 in the denominator in equation 1.2 is replaced with P_1 .

With a volumetric flow rate Q_w representing non-compressive fluid such as water, oil, etc. the following equation is applied;

$$Q_w = \frac{\pi R^4 (P_1 - P_2)}{8\eta_w \ell} \text{-----(1.3)}$$

Q_a : Volumetric flow rate of compressive fluid (air) under pressure P_2 (mL/s)

Q_w : Volumetric flow rate of non-compressive fluid (mL/s)

P_1 : Primary (test) pressure

(when negative pressure, atmospheric pressure) (Pa)

P_2 : Secondary (test) pressure

(when negative pressure, test pressure) (Pa)

R : Radius of the opening (cm)

ℓ : Length of the opening (cm)

η_a : Viscosity of compressive fluid (Pa · s)

η_w : Viscosity of non-compressive fluid (Pa · s)

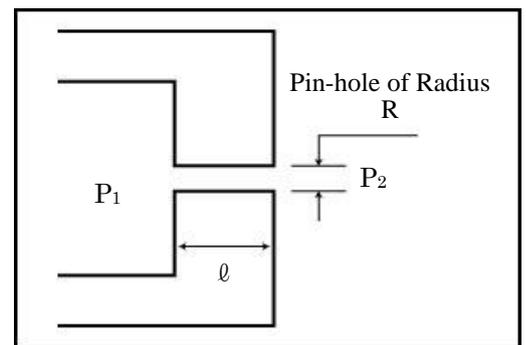


Fig. 1.2 Theoretic Model of Leakage

The relationship of volumetric flow rate influenced by the difference between gaseous fluid and liquid, and between two pressures with the same test piece is shown in Table 1.3. Refer to equations 1.1 and 1.2.

Table 1.3 Relationship between Leak Volume vs. Test Pressure and Viscosity

	Condition	Relative Equation
Gas	The ratio of leak volume to the different test pressures towards the same gas.	$\frac{Q_{ax}}{Q_{ay}} = \frac{P_{1x}^2 - P_{2x}^2}{P_{1y}^2 - P_{2y}^2}$
	The ratio of leak volume to the fixed test pressures towards different gases.	$\frac{Q_{ax}}{Q_{ay}} = \frac{\eta_{ay}}{\eta_{ax}}$
	The ratio of leak volume to the different test pressures towards different gases.	$\frac{Q_{ax}}{Q_{ay}} = \frac{\eta_{ay}}{\eta_{ax}} \times \frac{P_{1x}^2 - P_{2x}^2}{P_{1y}^2 - P_{2y}^2}$
Fluid	The ratio of leak volume to the different test pressures towards the same liquid.	$\frac{Q_{wx}}{Q_{wy}} = \frac{P_{1x} - P_{2x}}{P_{1y} - P_{2y}}$
	The ratio of leak volume to the fixed test pressure towards different liquids.	$\frac{Q_{wx}}{Q_{wy}} = \frac{\eta_{wy}}{\eta_{wx}}$
	The ratio of leak volume to the different test pressures towards different liquids.	$\frac{Q_{wx}}{Q_{wy}} = \frac{\eta_{wy}}{\eta_{wx}} \times \frac{P_{1x} - P_{2x}}{P_{1y} - P_{2y}}$
Gas/ Liquid	The ratio of leak volume to the different test pressures towards different gases and liquids.	$\frac{Q_{ax}}{Q_{wy}} = \frac{\eta_{wy}}{2\eta_{ax}} \times \frac{(P_{1x}^2 - P_{2x}^2)}{P_{2x}(P_{1y} - P_{2y})}$
	The ratio of leak volume to the fixed test pressure towards different gases and liquids.	$\frac{Q_{ax}}{Q_{wy}} = \frac{\eta_{wy}}{2\eta_{ax}} \times \frac{(P_1 + P_2)}{P_2}$

Viscosity (Viscosity Coefficient) η

Viscosity is one of the important factors when handling fluid. Different units are used in different fields. Here are some examples;

$$1\text{Pa} \cdot \text{s} = 1\text{N} \cdot \text{s} \cdot \text{m}^{-2} = 1.02 \cdot 10^{-5}\text{kgf} \cdot \text{s} \cdot \text{cm}^{-2} = 10\text{P}$$

P:Poise

N:Newton

$\text{kgf} \cdot \text{s} \cdot \text{cm}^{-2}$: Engineering Unit
(kgf second per square centimeter)

Pa: Pascal

Also, to represent kinematical viscosity of the fluid, use the equation;

$$\gamma = \eta / \rho$$

But ρ is the density of the fluid.

Some examples of the viscosity coefficients for air, water, brake oil and gasoline are shown in Table 1.4.

Table 1.4 Viscosity Coefficient of Gases and Liquids

Fluid	Temperature	Viscosity
Air	0°C	$1.71 \times 10^{-5} \text{Pa} \cdot \text{s}$
	20°C	$1.81 \times 10^{-5} \text{Pa} \cdot \text{s}$
	50°C	$1.95 \times 10^{-5} \text{Pa} \cdot \text{s}$
	70°C	$2.04 \times 10^{-5} \text{Pa} \cdot \text{s}$
Water	0°C	$1.79 \times 10^{-3} \text{Pa} \cdot \text{s}$
	20°C	$1.00 \times 10^{-3} \text{Pa} \cdot \text{s}$
	50°C	$0.55 \times 10^{-3} \text{Pa} \cdot \text{s}$
	70°C	$0.40 \times 10^{-3} \text{Pa} \cdot \text{s}$
Brake Oil	20°C	$2.6 \times 10^{-2} \text{Pa} \cdot \text{s}$
	50°C	$1.0 \times 10^{-2} \text{Pa} \cdot \text{s}$
	70°C	$0.7 \times 10^{-2} \text{Pa} \cdot \text{s}$
Gasoline	20°C	$6.0 \times 10^{-4} \text{Pa} \cdot \text{s}$

Leak Rate Calculation Using a Variety of Units of the Viscosity Coefficient (Pressure: Absolute Pressure)

(1) Calculation of Leak Rate in Compressive Fluid

Using equation 1.2, volumetric flow rates of compressive fluid based on a variety of calculations units are summarized in Table 1.5.

Table 1.5 Leak Rate of Compressive Fluid

a	R: (m); ℓ : (m); η_a : ($\text{Pa} \cdot \text{s}$); P_1, P_2 : (Pa) $Q (\text{m}^3 / \text{s}) = 3.927 \times 10^{-1} \frac{R^4}{\ell \eta_a} \times \frac{P_1 + P_2}{2} \times \frac{P_1 - P_2}{P_2}$
b	R: (cm); ℓ : (cm); η_a : ($\text{Pa} \cdot \text{s}$); P_1, P_2 : (Pa) $Q (\text{ml} / \text{s}) = 3.927 \times 10^{-1} \frac{R^4}{\ell \eta_a} \times \frac{P_1 + P_2}{2} \times \frac{P_1 - P_2}{P_2}$
c	R: (cm); ℓ : (cm); η_a : ($\text{kg} \cdot \text{s} / \text{cm}^2$); P_1, P_2 : (kg / cm^2) $Q (\text{ml} / \text{s}) = 3.927 \times 10^{-1} \frac{R^4}{\ell \eta_a} \times \frac{P_1 + P_2}{2} \times \frac{P_1 - P_2}{P_2}$
d	R: (cm); ℓ : (cm); η_a : ($P = \frac{1}{9.80665 \times 10^5} \text{kg} \cdot \text{s} / \text{cm}^2$); P_1, P_2 : (kg / cm^2) $Q (\text{ml} / \text{s}) = 3.851 \times 10^5 \frac{R^4}{\ell \eta_a} \times \frac{P_1 + P_2}{2} \times \frac{P_1 - P_2}{P_2}$

Note: R: Radius of Pipe, ℓ : Length of Pipe, η_a : Viscosity of Fluid, P_1 : Primary Absolute Pressure, P_2 : Secondary Absolute Pressure

(2) Calculation of Leak Rate in Non-Compressive Fluid

Using equation 1.3, volumetric flow rates of non-compressive fluid based on a variety of calculation units are summarized in Table 1.6

Table 1.6 Leak Rate of Non-compressive Fluid

a	<p>R: (m); ℓ: (m); η_w: (Pa · s); P₁, P₂: (Pa)</p> $Q(\text{m}^3/\text{s}) = 3.927 \times 10^{-1} \frac{R^4}{\ell \eta_w} \times (P_1 - P_2)$
b	<p>R: (cm); ℓ: (cm); η_w: (Pa · s); P₁, P₂: (Pa)</p> $Q(\text{ml}/\text{s}) = 3.927 \times 10^{-1} \frac{R^4}{\ell \eta_w} \times (P_1 - P_2)$
c	<p>R: (m); ℓ: (cm); η_w: (kg · s/cm²); P₁, P₂: (kg/cm²)</p> $Q(\text{ml}/\text{s}) = 3.927 \times 10^{-1} \frac{R^4}{\ell \eta_w} \times (P_1 - P_2)$
d	<p>R: (cm); ℓ: (cm); η_a: (P = $\frac{1}{9.80665 \times 10^5}$ kg · s/cm²); P₁, P₂: (kg/cm²)</p> $Q(\text{ml}/\text{s}) = 3.851 \times 10^5 \frac{R^4}{\ell \eta_w} \times (P_1 - P_2)$

R: Radius of Pipe, ℓ: Length of Pipe, η_w: Viscosity of Fluid,
P₁: Primary Absolute Pressure, P₂: Secondary Absolute Pressure

Leak Rate Conversion from Air to Liquid

Using Table 1.2 and Table 1.3 the leak rates of water, gasoline, and brake oil in reference to air are calculated, provided that the same test piece is used. The temperature of fluid is kept fixed at 20°C, and the test pressure is kept at the same level. The results are as shown Fig. 1.3.

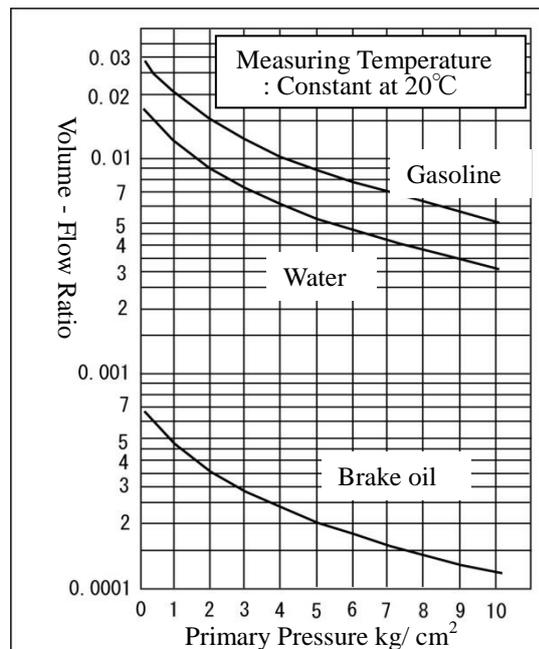


Fig. 1.3 Volumetric Flow Rate of Fluid Referred to Air

Calculation of Orifice model

$$Q = \varepsilon \times \alpha \times A \times (2 \times (P1 - P2) / \rho)^{1/2}$$

Q: Air volume flow rate

ε : Expansion compensation coefficient

α : Flow coefficient

A : Area of the hole

P1 : Upward pressure abs

P2 : Downward pressure abs

ρ : Air density